

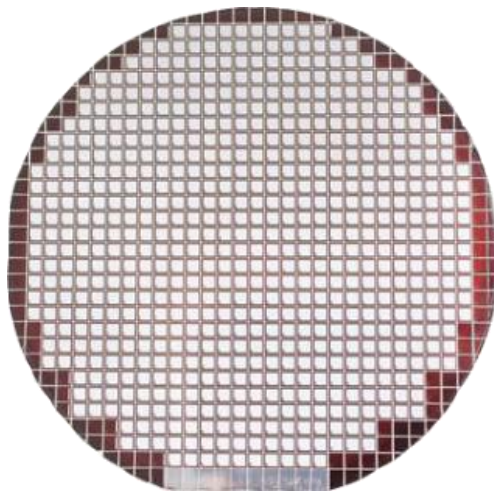


# *FEM simulation applied to Thermal Laser Separation (TLS) with Deep Scribe for Silicon Wafer Dicing*

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- Motivation
- Principles of
  - Thermal Laser Separation
  - Deep Scribe
- FEM Simulation of Deep Scribe
- Experiments and Results
  - Parameter Study
  - Breaking Strength
- Conclusions

## How to separate a wafer into single chips?

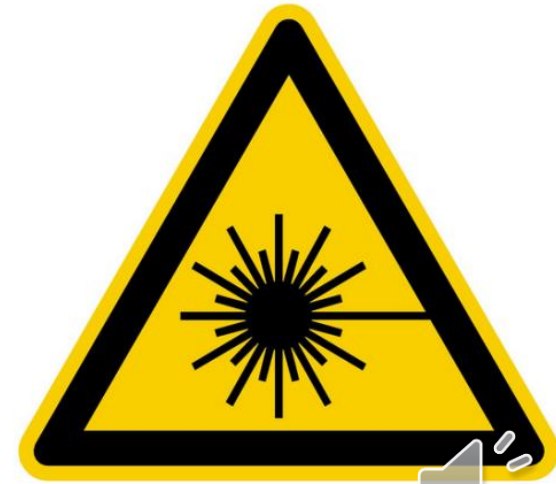


[Karl O. Dohnke]

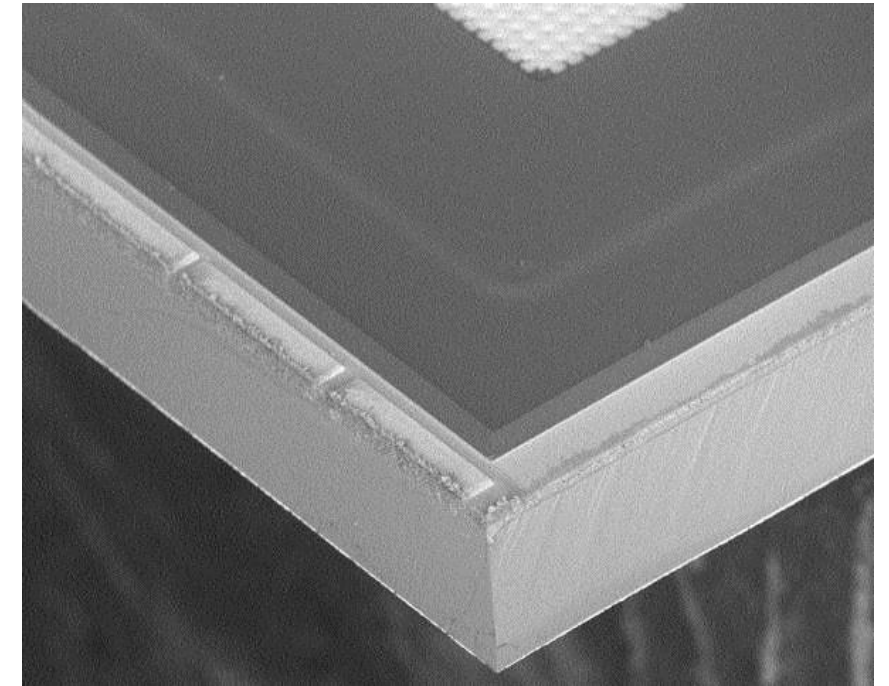


- Established methods
  - E.g. Mechanical Blade Dicing, Laser Ablation, ...
- Requirements depend on product
- Reduction cost of ownership
- Maximization of throughput and yield

**Laser processes become more relevant**

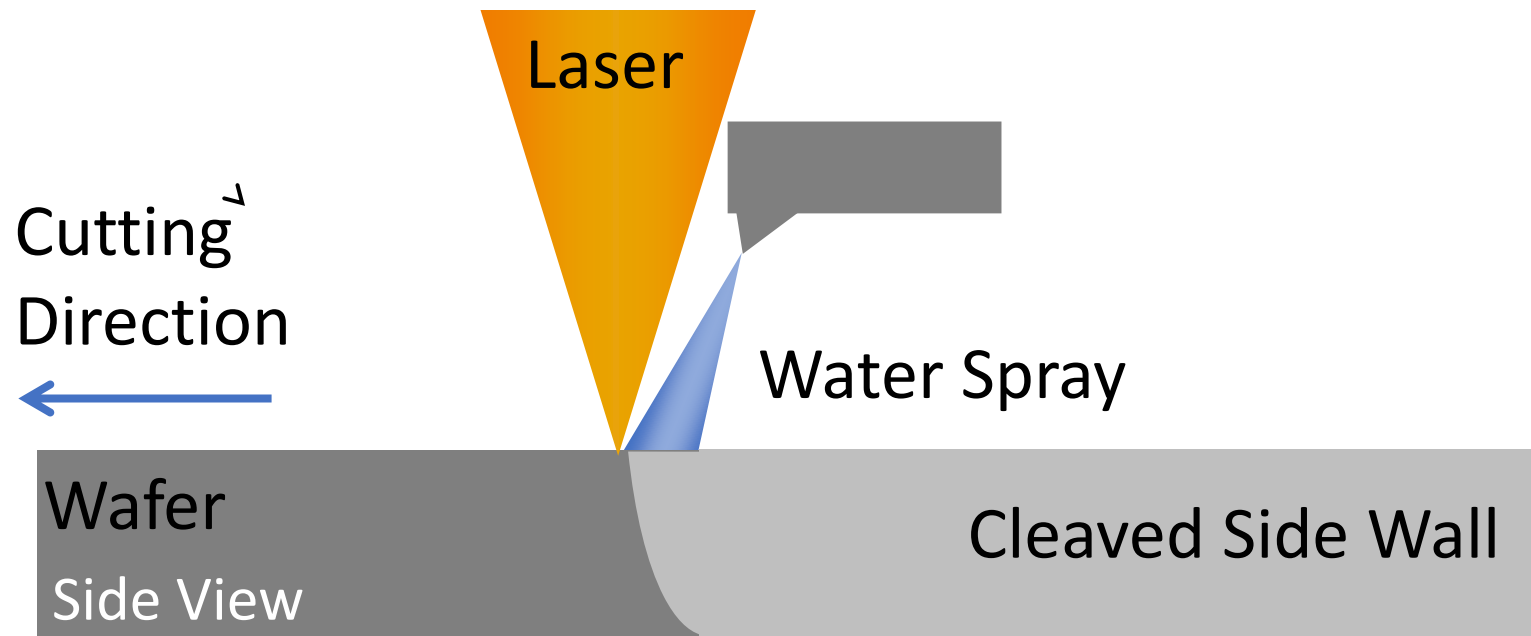


- Two steps (Scribe & Cleave)
- Contact-less & zero kerf
- Feed rates up to 400 mm/s
- High edge quality
- Low cost of ownership

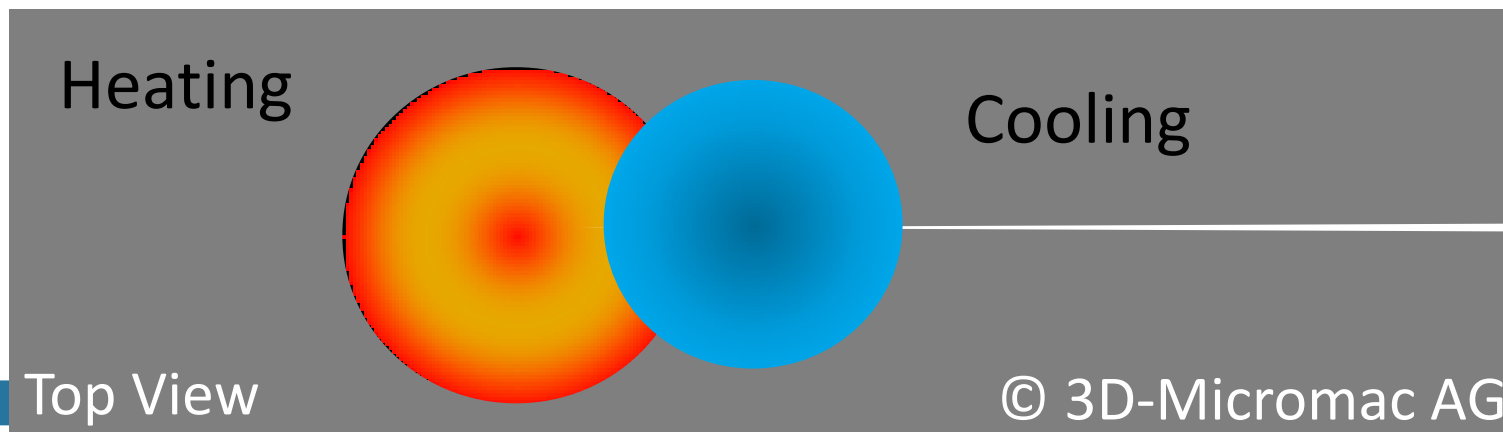


JFET on  $\mu$ 4H-SiC-Wafer,  
Thickness 160 m

→ Complex process, absorption depended



Thermal induced mechanical stresses creating and guiding a crack

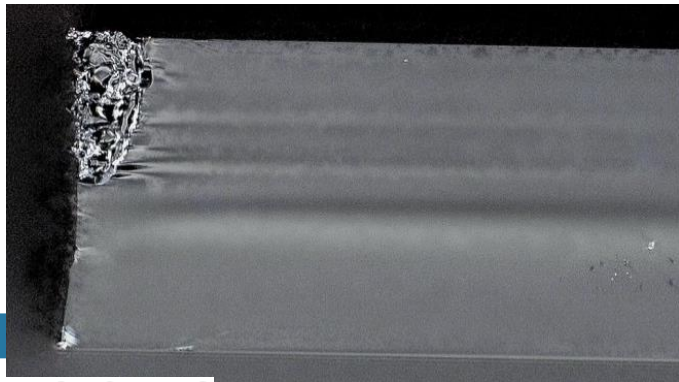
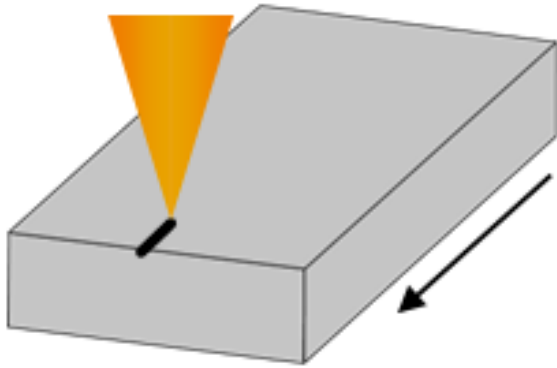


Starting point defined by scribe step

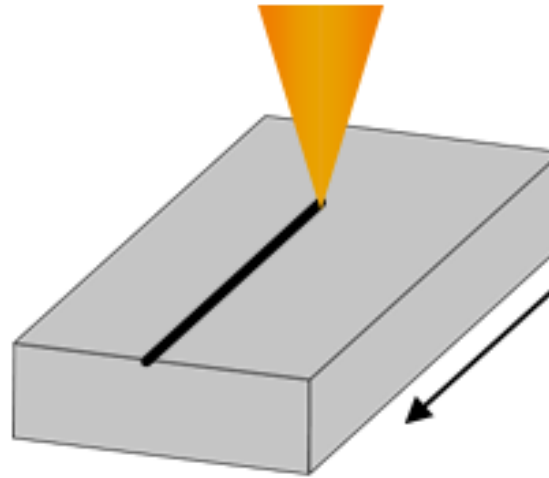
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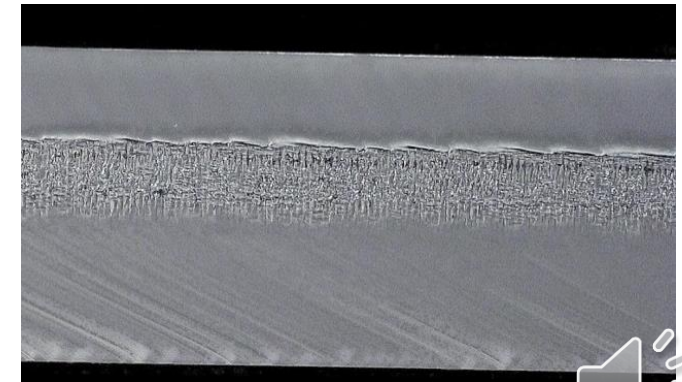
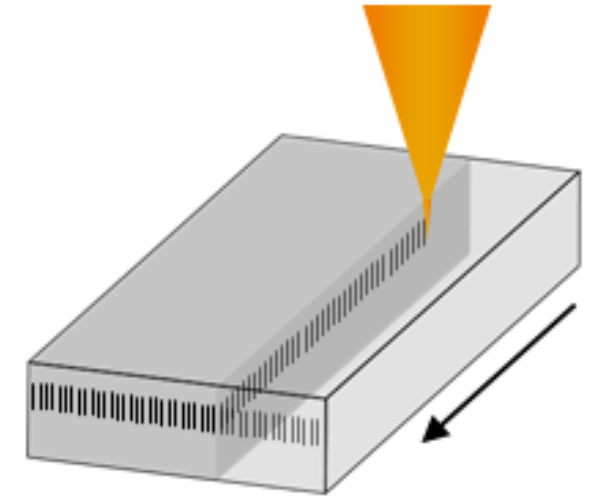
## Initial Scribe



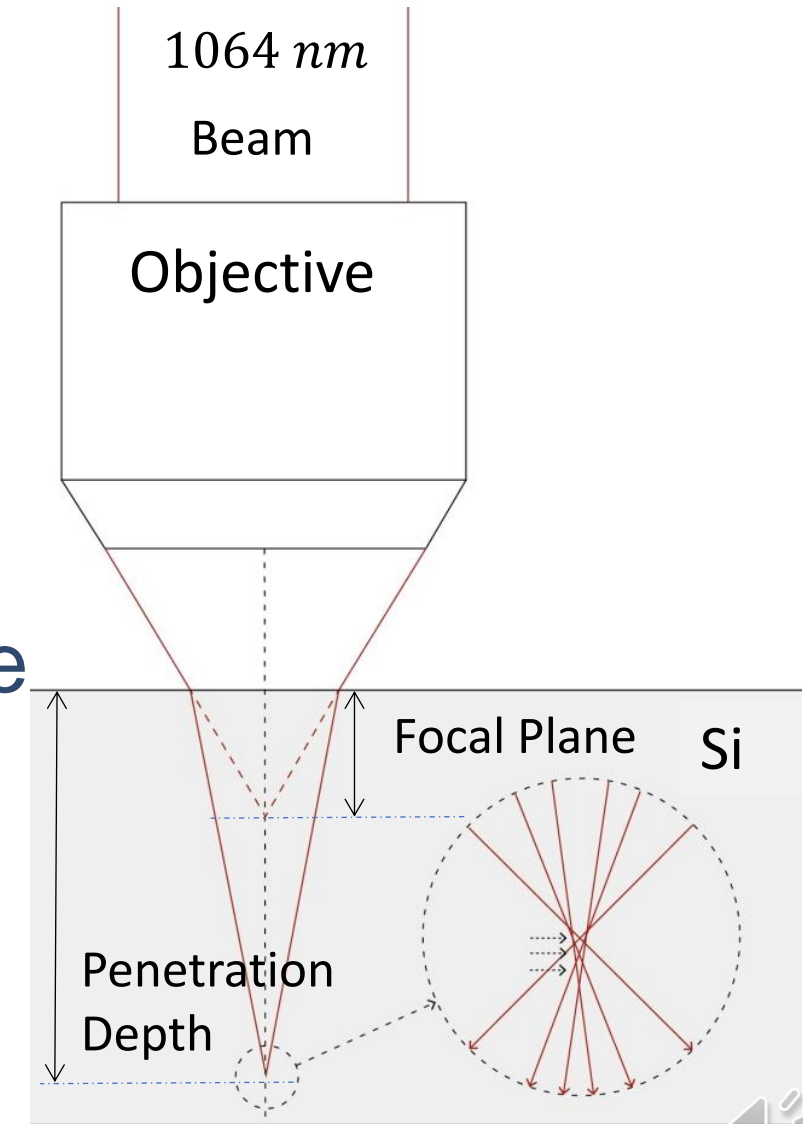
## Continuous Scribe



## Deep Scribe

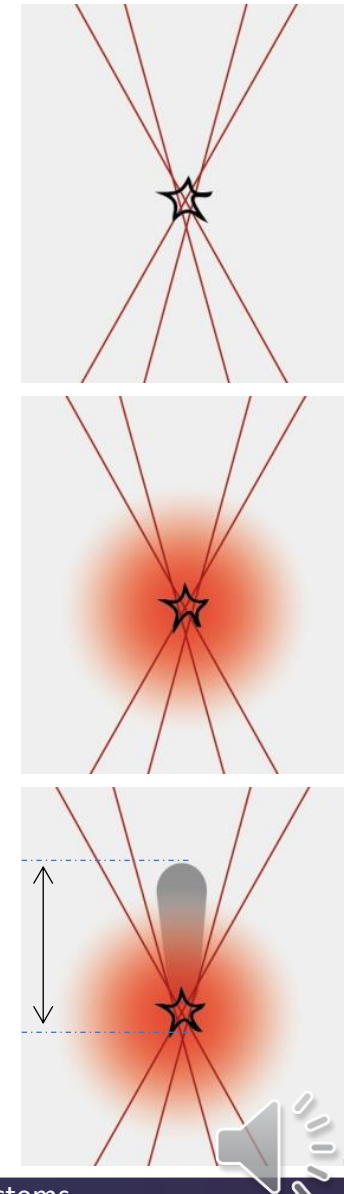
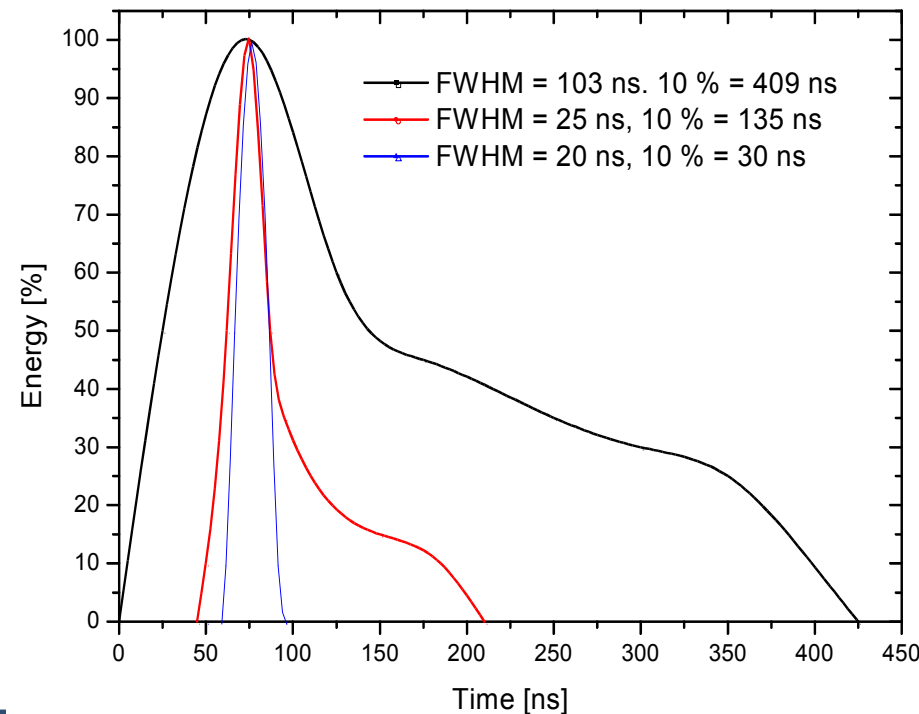


- Conservation:  $R+A+T=1$
- Influence of surface
  - Reflection ( $R = 0.35$ )
  - Refraction ( $n_{Si} = 3.56$ )
  - Spherical aberration
- Enlargement of focal length and spot size
- Increasing depth - decreasing power
- Fluence at focal plane  $\gg$  surface



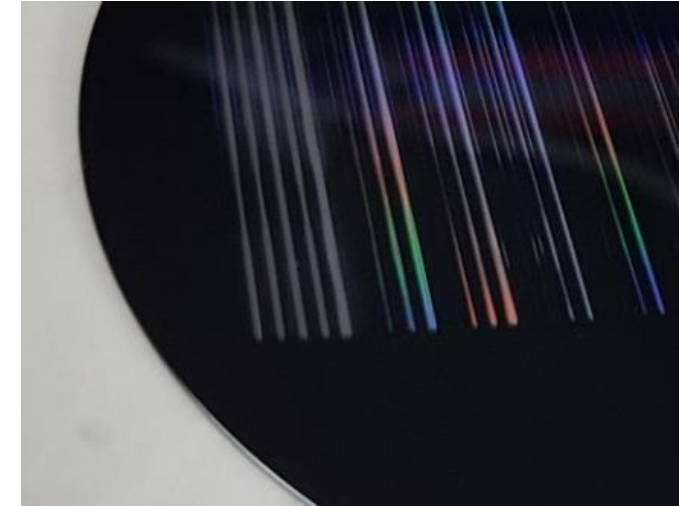


- Reaching threshold fluence
- Spontaneous increase of absorption
- Generating of free charge carriers
- Rising of temperature  $\rightarrow$  lattice absorption
- Heat conduction
- Melting along caustic
- Modification depends on shape & duration of pulses



# Requirements for Deep Scribe

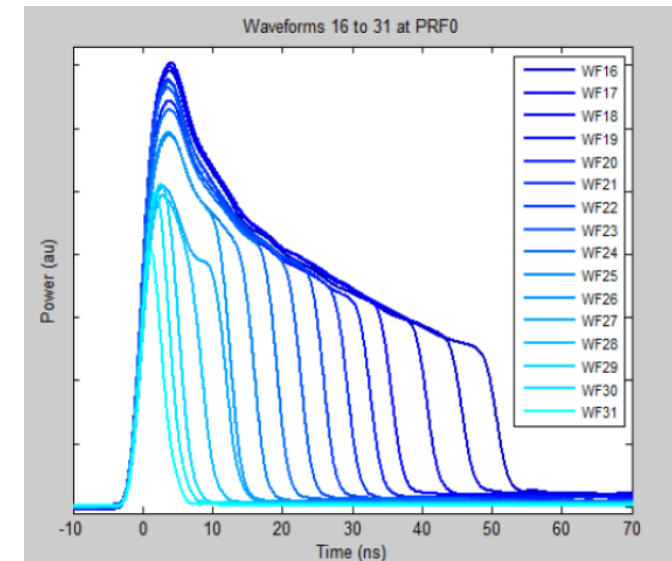
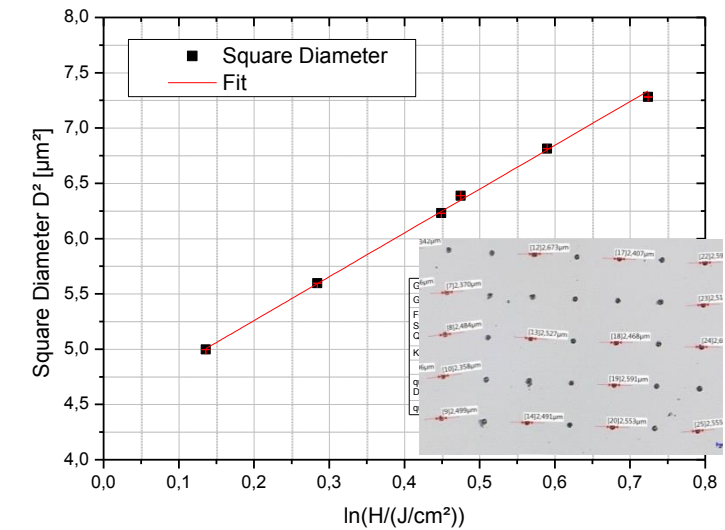
- Material properties
  - Polished surface, doping  $<10^{20} \text{ cm}^{-3}$
- Optical setup
  - $NA = 0.65$ , correction of spherical aberrations
- 1064 nm Laser
  - Sufficient shape & duration of pulses
- Correction of focal height
  - Measurement of topography
- Vibration damping of system



- Multiphysical model using Octave
- Simulation of a single pulse
- Two-dimensional model in polar coordinates
- Parameter:  $E_p, t_p - w_0, z$
- Determination of the modification length
- Program Sequence

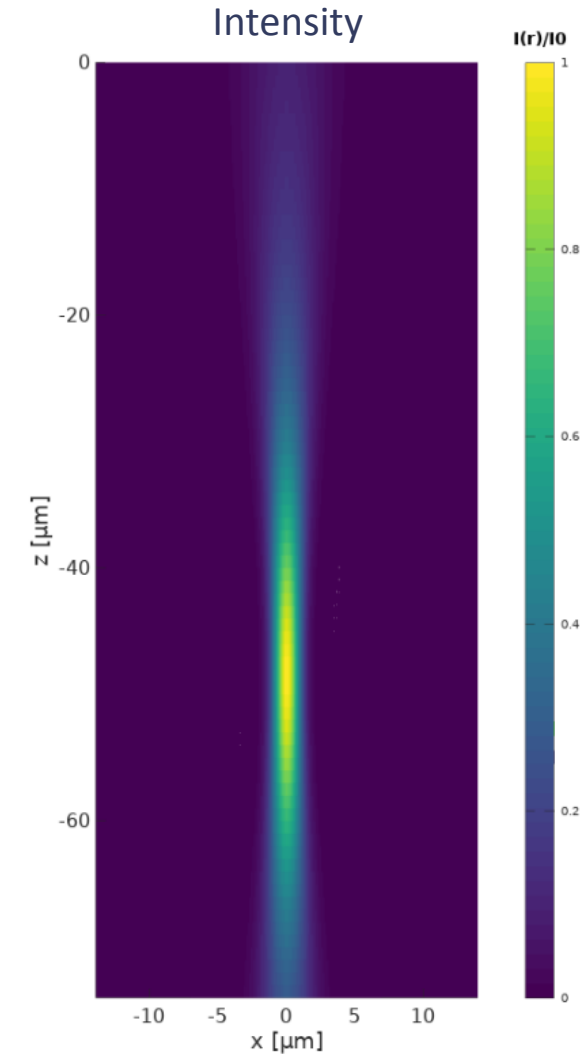


- Calculation of beam caustic  $w(z) = w_0 \cdot \sqrt{1 + \left(\frac{z \cdot \lambda \cdot M^2}{n_{Si} \cdot \pi \cdot w_0^2}\right)^2}$
- Verification spot size via LIU Plot
  - *calc*:  $2w_0 = 2.35 \mu\text{m}$  *vs.* *LIU*:  $2w_0 = 2.8 \mu\text{m} \pm 0.3 \mu\text{m}$
- Function fitting for various pulse shapes



- Function fitting for temperature dependent material parameters
  - Absorption coefficient  $\alpha$
  - Specific heat capacity  $C_p$
  - Thermal conductivity  $\lambda$
- Neglecting of variability for
  - Reflection  $R = 0.35$  (nonpolar,  $<40^\circ$ )
  - Refraction
  - Density



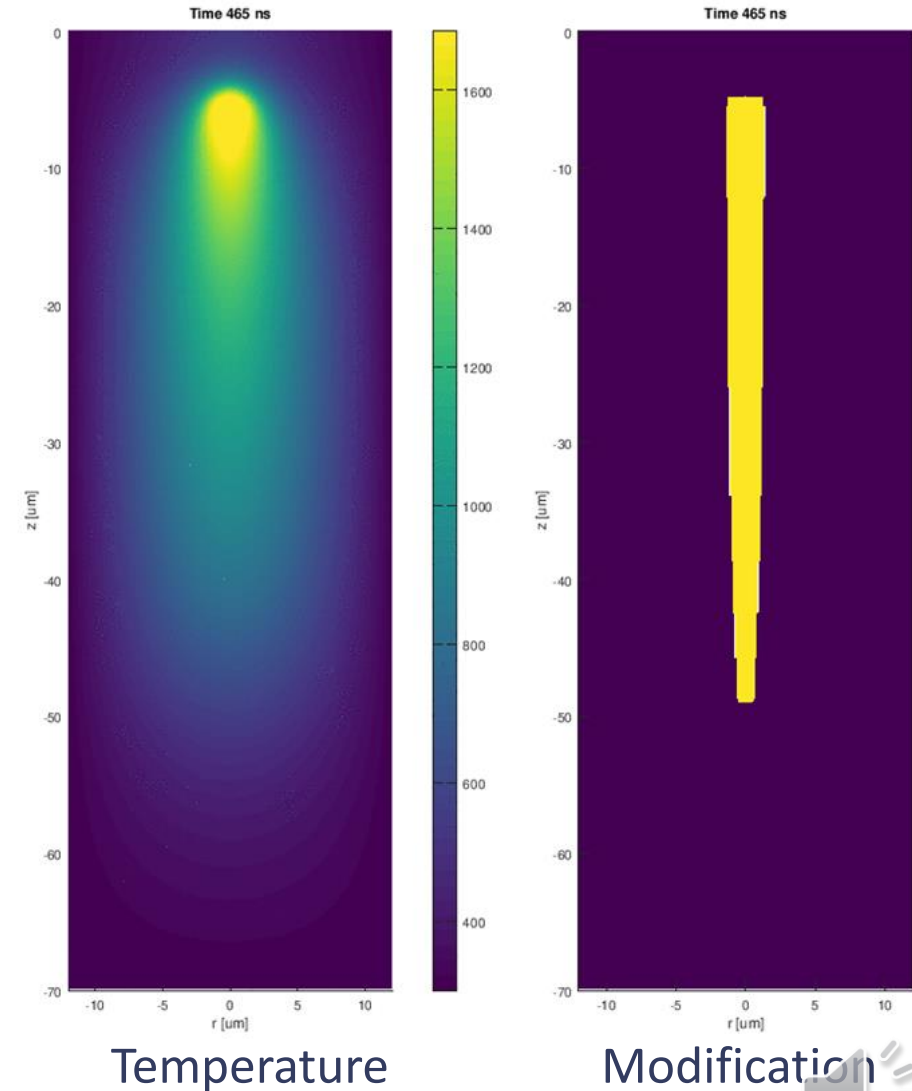
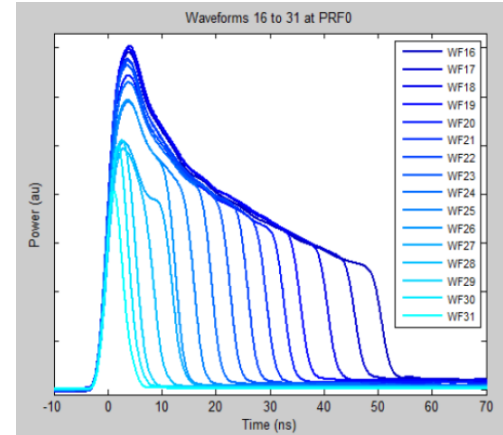


- Calculation of laser energy for the step
- Surface reflection  $R = 0.35$  (nonpolar,  $<40^\circ$ )
- Maximum of intensity  $I_0(z = 0)$   $I_0(t) = \frac{2 \cdot E(t)}{\Delta t \cdot \pi \cdot w_0^2}$
- Intensity distribution  $I(r, z) = \iint I_0 \cdot \left(\frac{w_0}{w(z)}\right)^2 \cdot e^{-\frac{2r^2}{w(z)^2}} dr dz$
- Layer absorption  $\Delta I(r, z) = I(r, z) \cdot (1 - e^{-\alpha(T) \cdot \Delta z})$
- Intensity loss  $I_0(z - 1) = I_0(z) - \sum \Delta I(z)$
- Thermalization  $\Delta T(r, z) = \frac{\Delta I(r, z) \cdot r^2 \cdot \Delta t}{c(T) \cdot M \cdot \rho}$
- Heat conduction
- Update of temperature dependent parameters

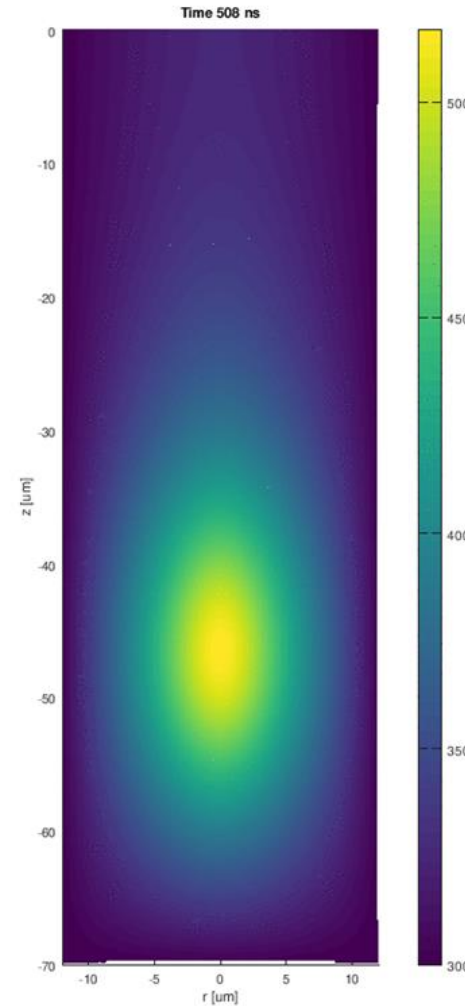
- Pulse duration:  $t = 500 \text{ ns}$
- Pulse energy:  $E_p = 5 \mu\text{J}$
- Focal position:  $z = 50 \mu\text{m}$

## Results:

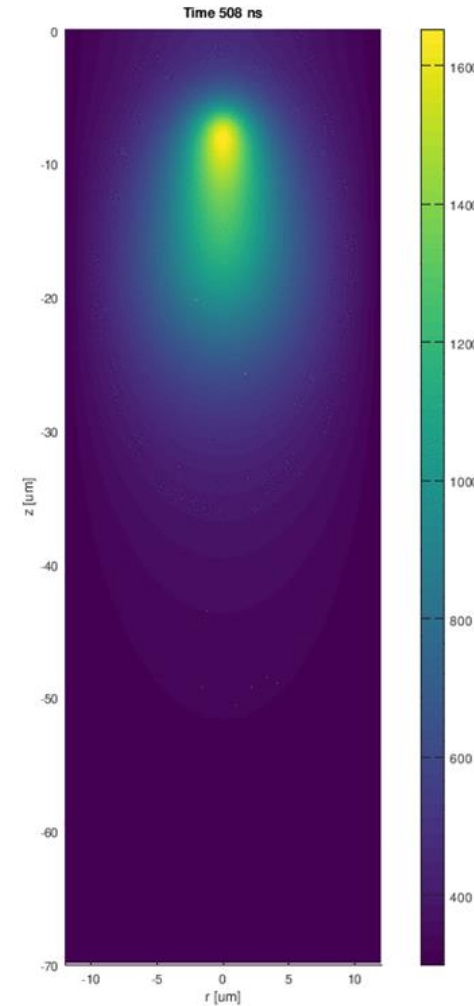
- Penetration depth:  $49 \mu\text{m}$
- Modification length:  $45 \mu\text{m}$
- Shape of the modification is plausible



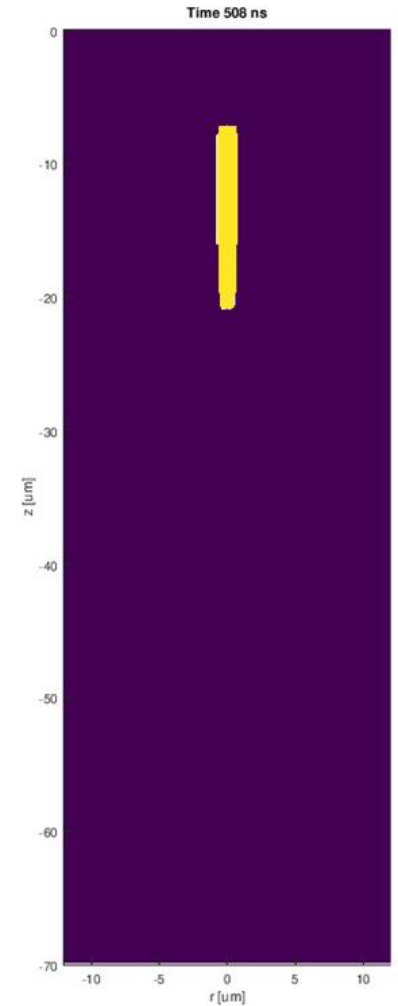
- Constant:  $E_p = 2.5 \mu\text{J}$
- Variation of focal position



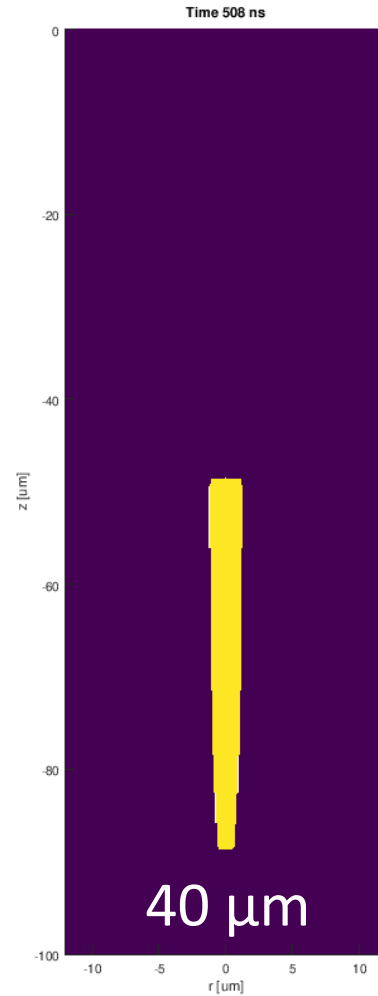
$z = 50 \mu\text{m}$



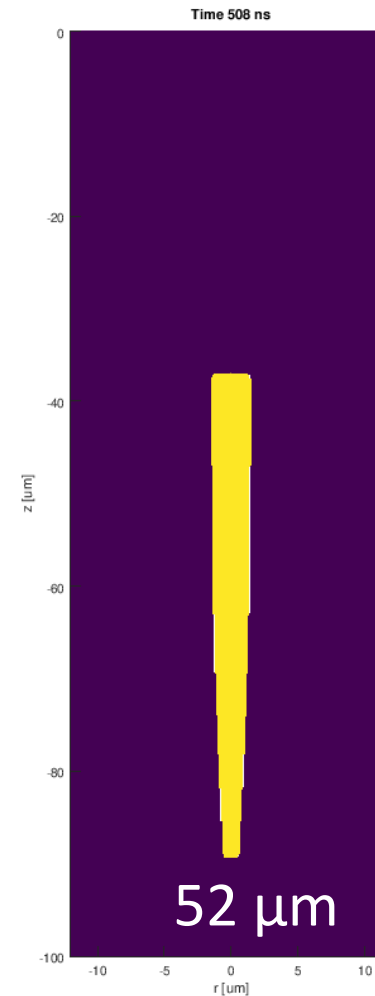
$z = 25 \mu\text{m}$



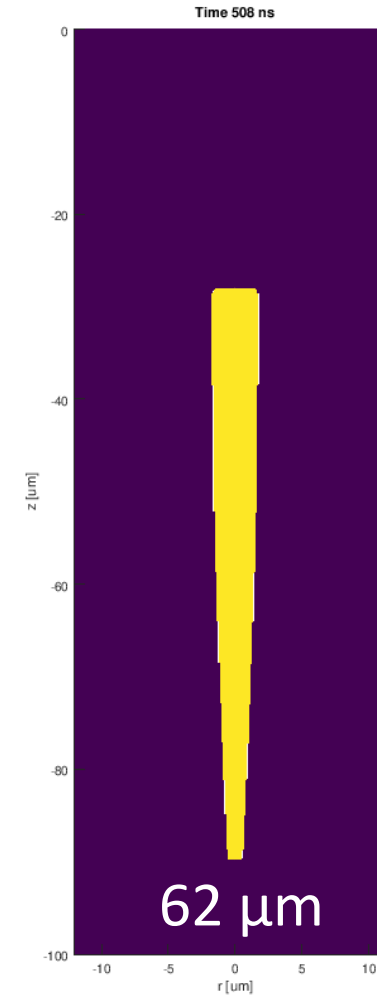
- Constant:  
 $z = 90 \mu m$
- Variation of  
pulse energy



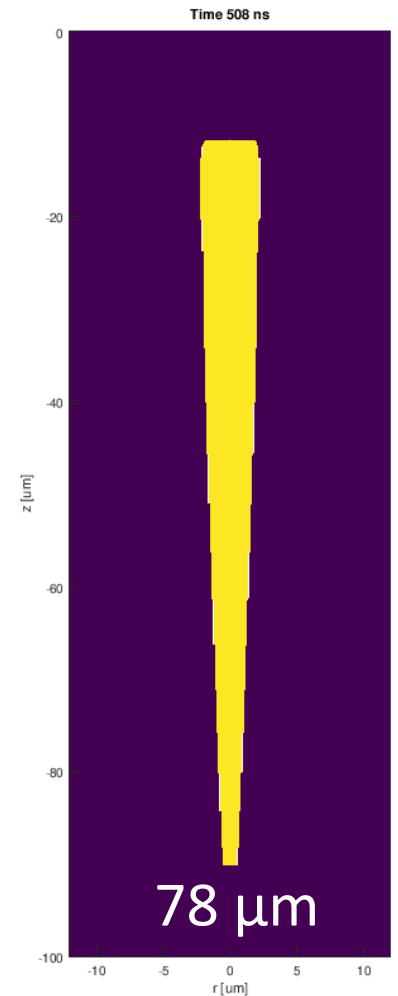
5  $\mu J$



7.5  $\mu J$



10  $\mu J$

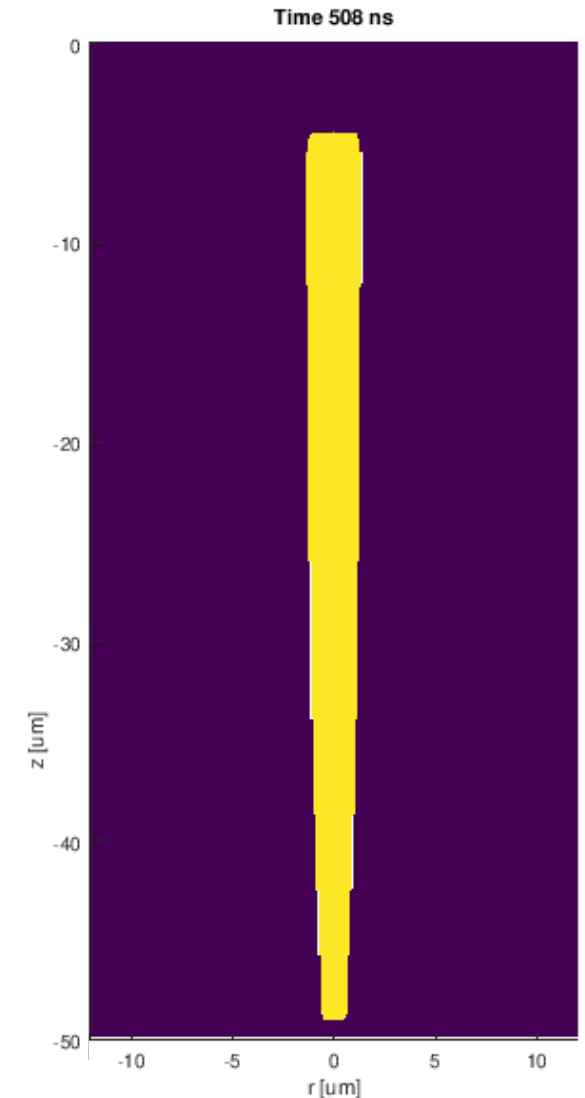


15  $\mu J$

- Creation of a FEM model with freeware
- Shape of the modification is plausible
- Correlations between parameters are confirmed
- Difference to experimental results
- Rough estimates of the result are possible

Further work:

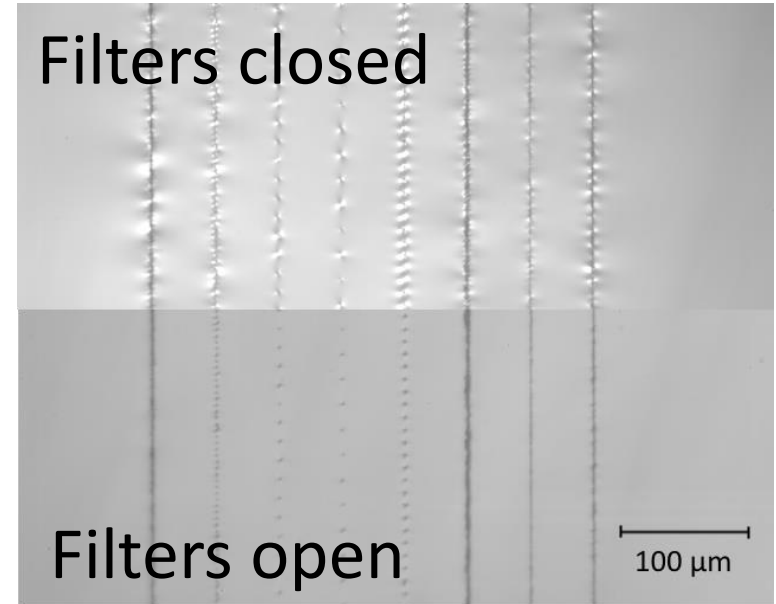
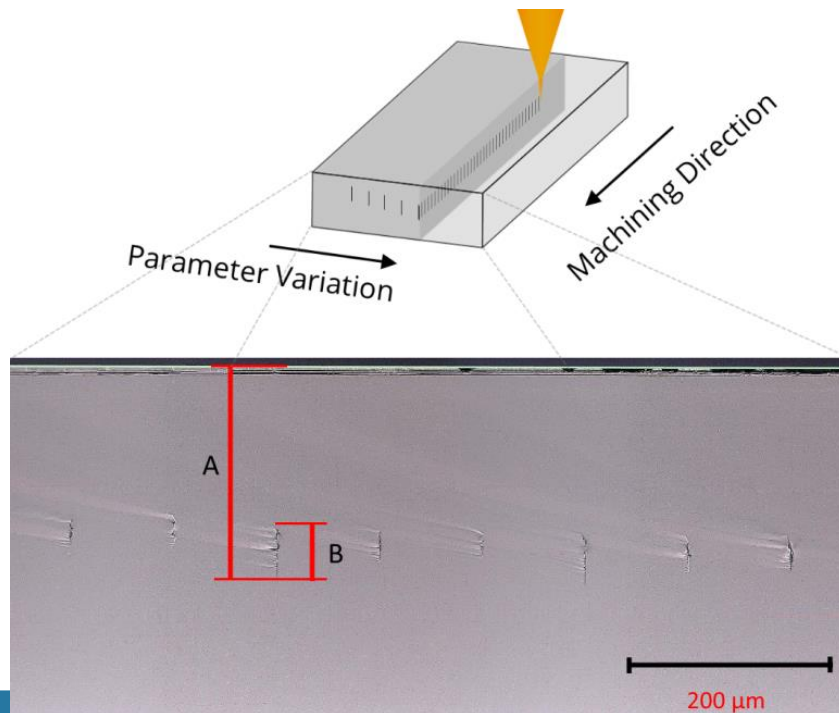
- Comparison with additional experiments
- Adjustment of absorption mechanism
- Interaction between multiple laser pulses





- Parameter variation of Deep Scribe
  - Variation of duration, distance, energy and position of pulses
- Combination of Deep Scribe and Cleave
- Investigation of breaking strength
  - 3-point bending test & Weibull analysis

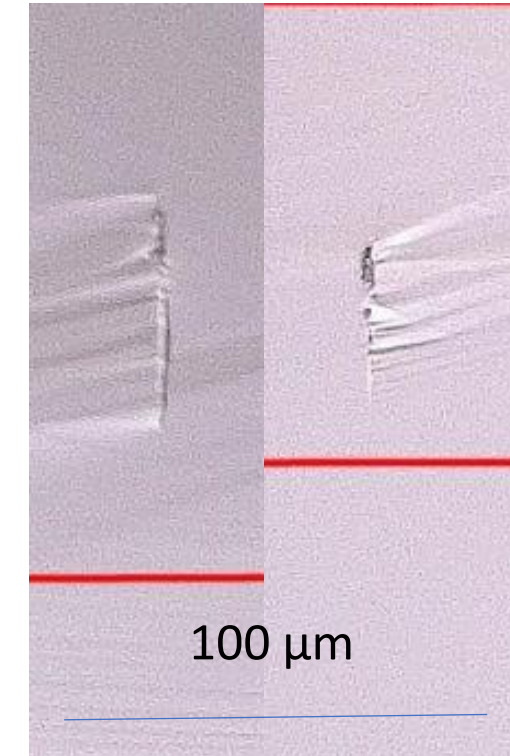
- In situ camera system
  - Polarizer & analyzer
  - Qualitative feedback deformation



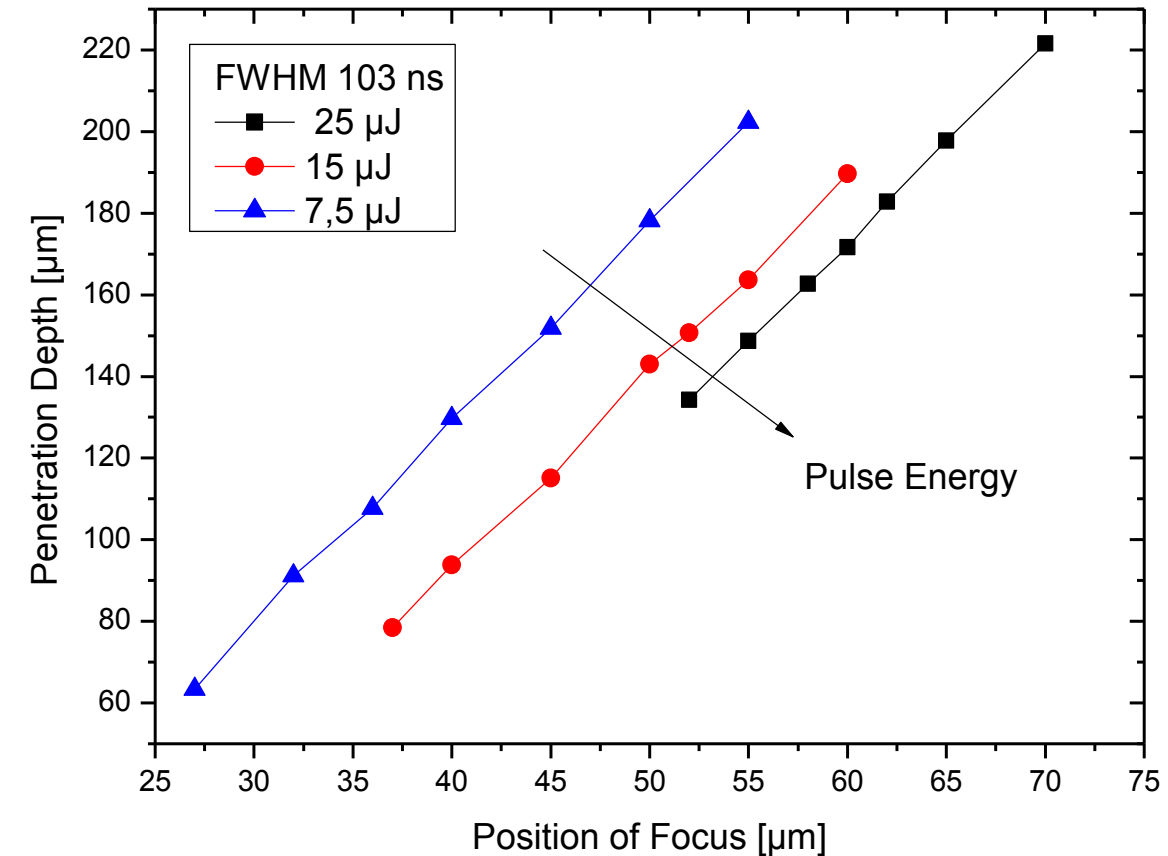
- Microscopic measurement of parameter variation
  - A: penetration depth
  - B: modification length

- Process window:
  - Pulse duration:  $> 26 \text{ ns}$
  - Energy:  $5 - 30 \mu\text{J}$
  - Modification length:  $15 - 75 \mu\text{m}$
  - Maximal penetration depth:  $0.9 \text{ mm}$
- Penetration depth = focal plane\*refractive index
- Decreasing pulse to pulse distance increasing damage of lattice

409 ns    202 ns



- Longer pulse durations Increasing modification length
- Increasing pulse energy  
Decreasing penetration depth
- Higher penetration depth  
Higher pulse energy necessary
- Increasing penetration depth reduction of modification length

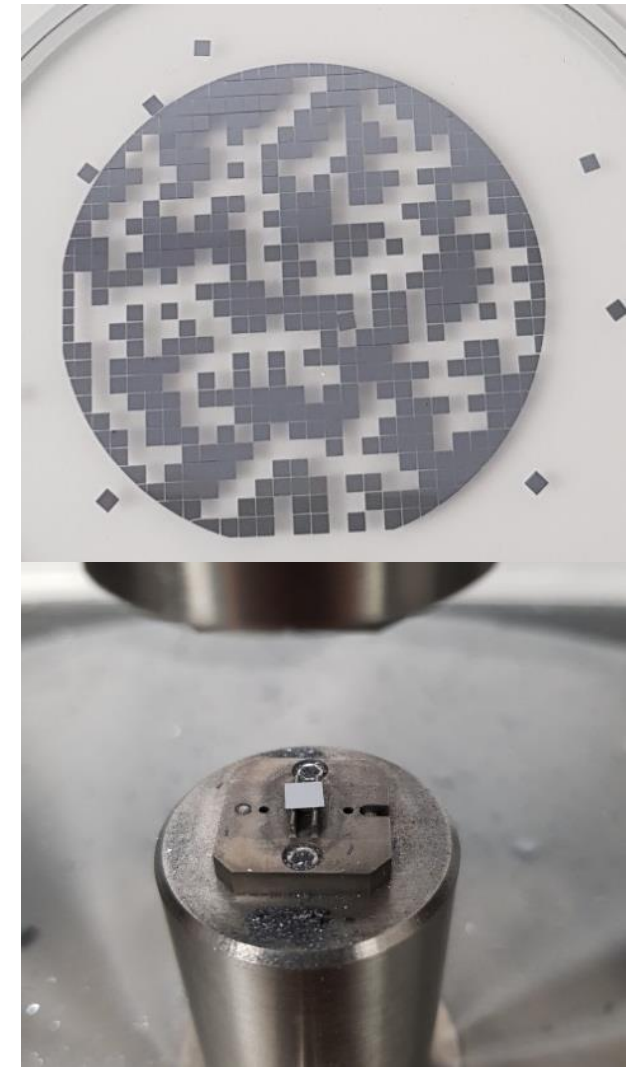


- Reduction of Cleave laser power
- Improved guiding properties
- Deviations  $< \pm 5 \mu m$
- Layers are stackable
- 1 Layer sufficient for 2 mm Si Wafer

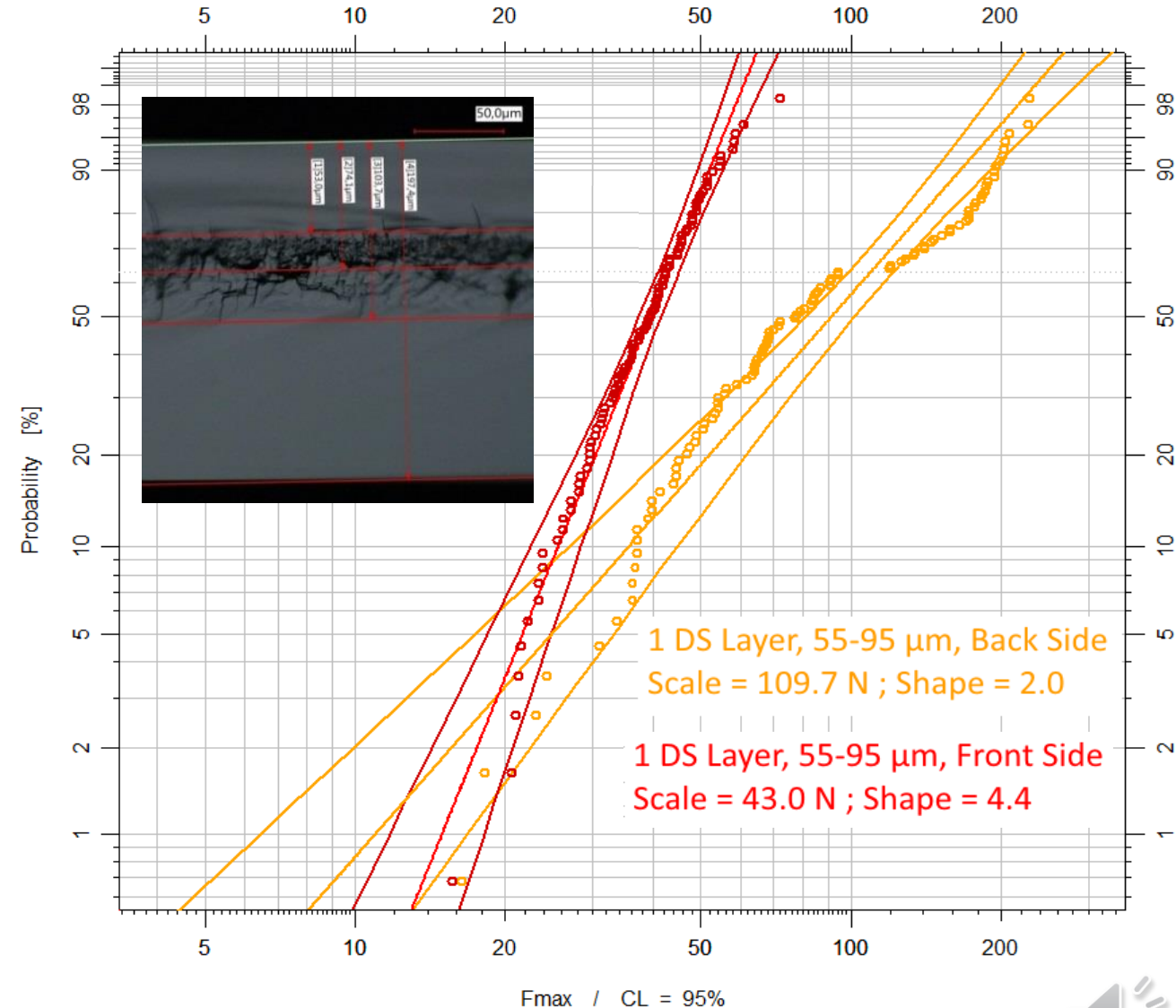




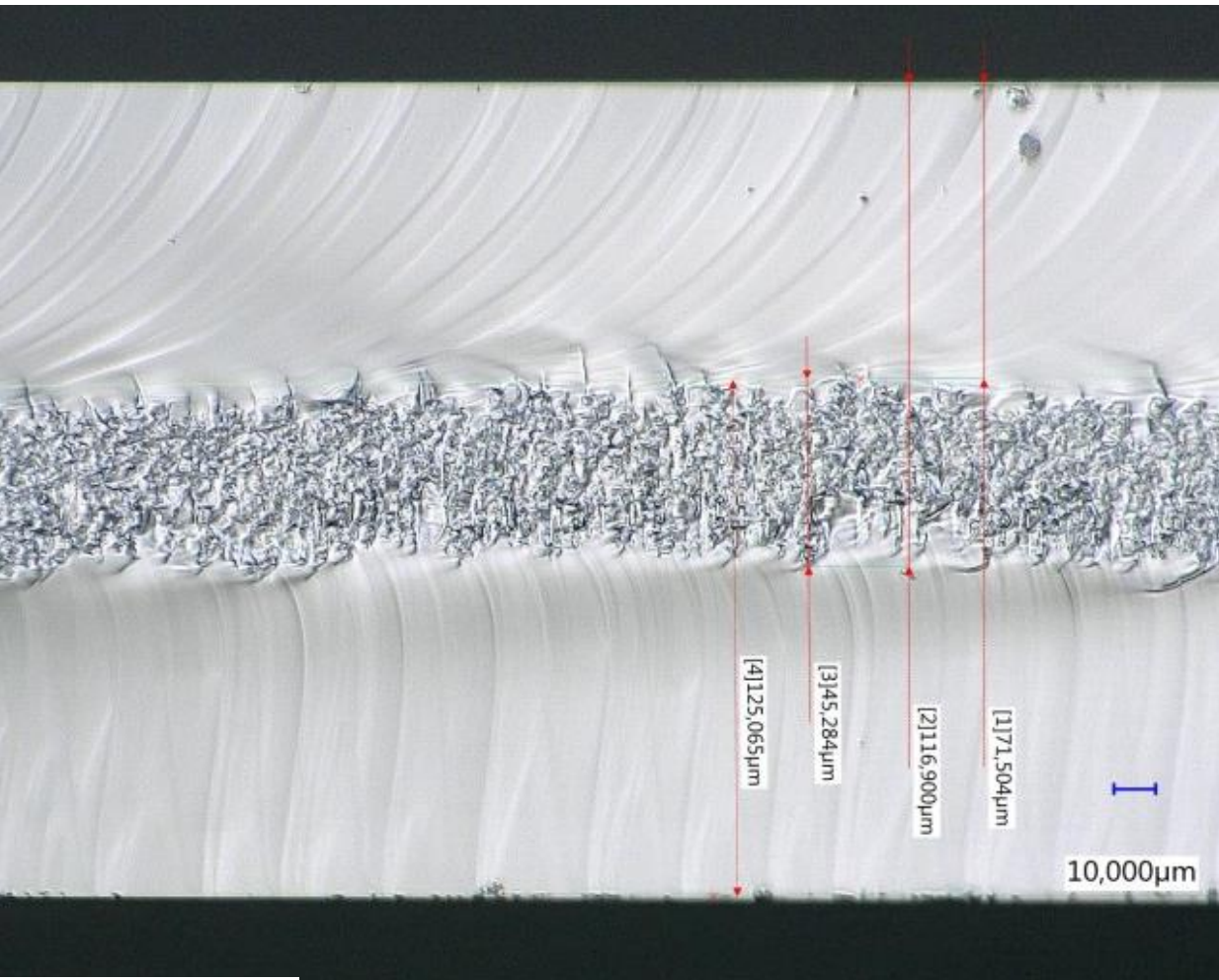
- Evidence about process stability
- Material: Si <100>, thickness 200  $\mu\text{m}$ , polished, p-type (Boron), 1 – 10  $\Omega \cdot \text{cm}$
- Chip size 3.6x3.6  $\text{mm}^2$
- 3-point bending test of 100 chips per site
- Weibull analysis – breakage of 63.21 %
- Optimization of breaking force and compared to mechanical sawing



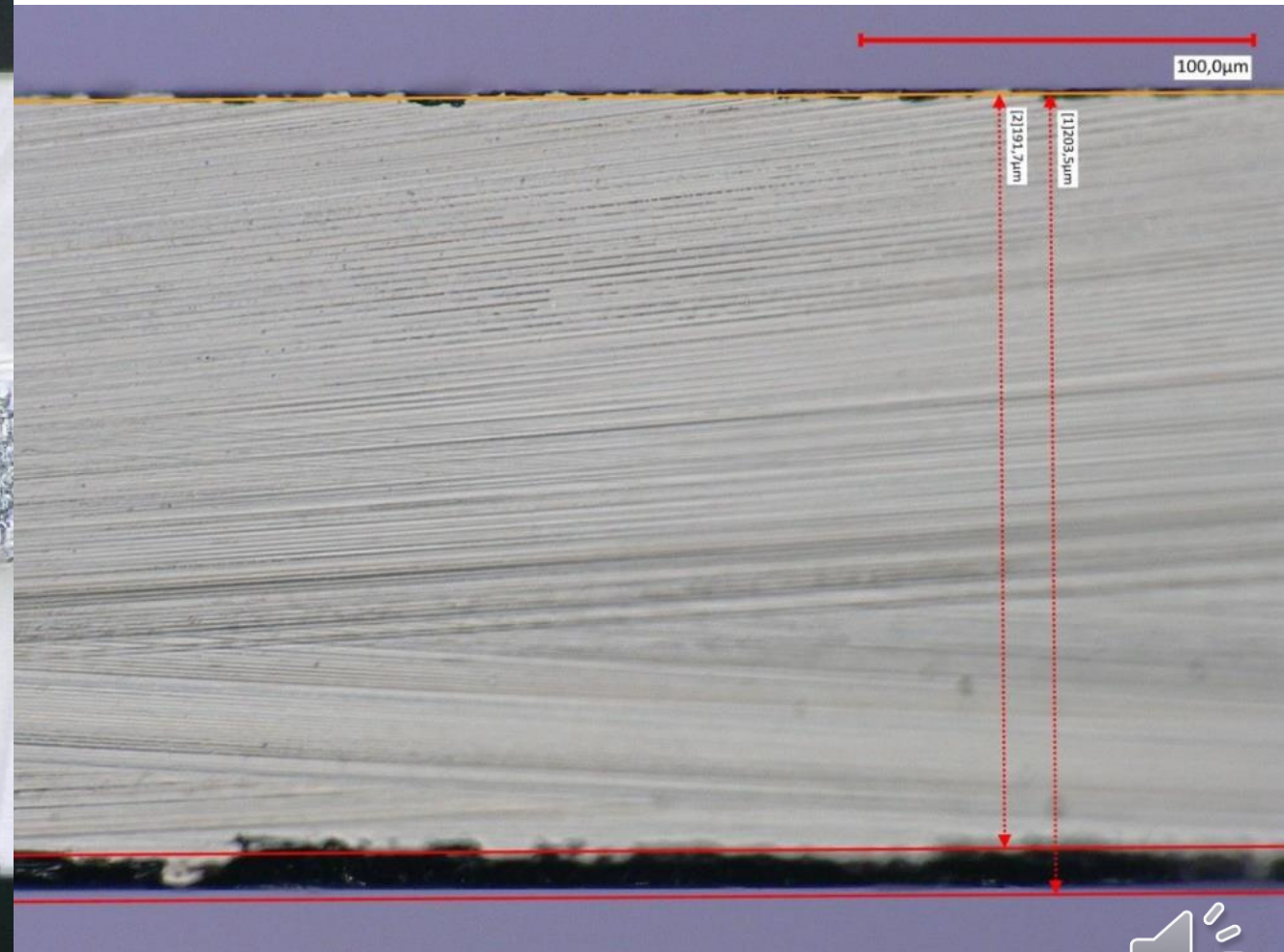
- Single Layer 55 – 95  $\mu m$
- 63,21 % value
  - Front: 43  $N$
  - Back: 109.7  $N$
- Reduction of front side forces



## Deep Scribe

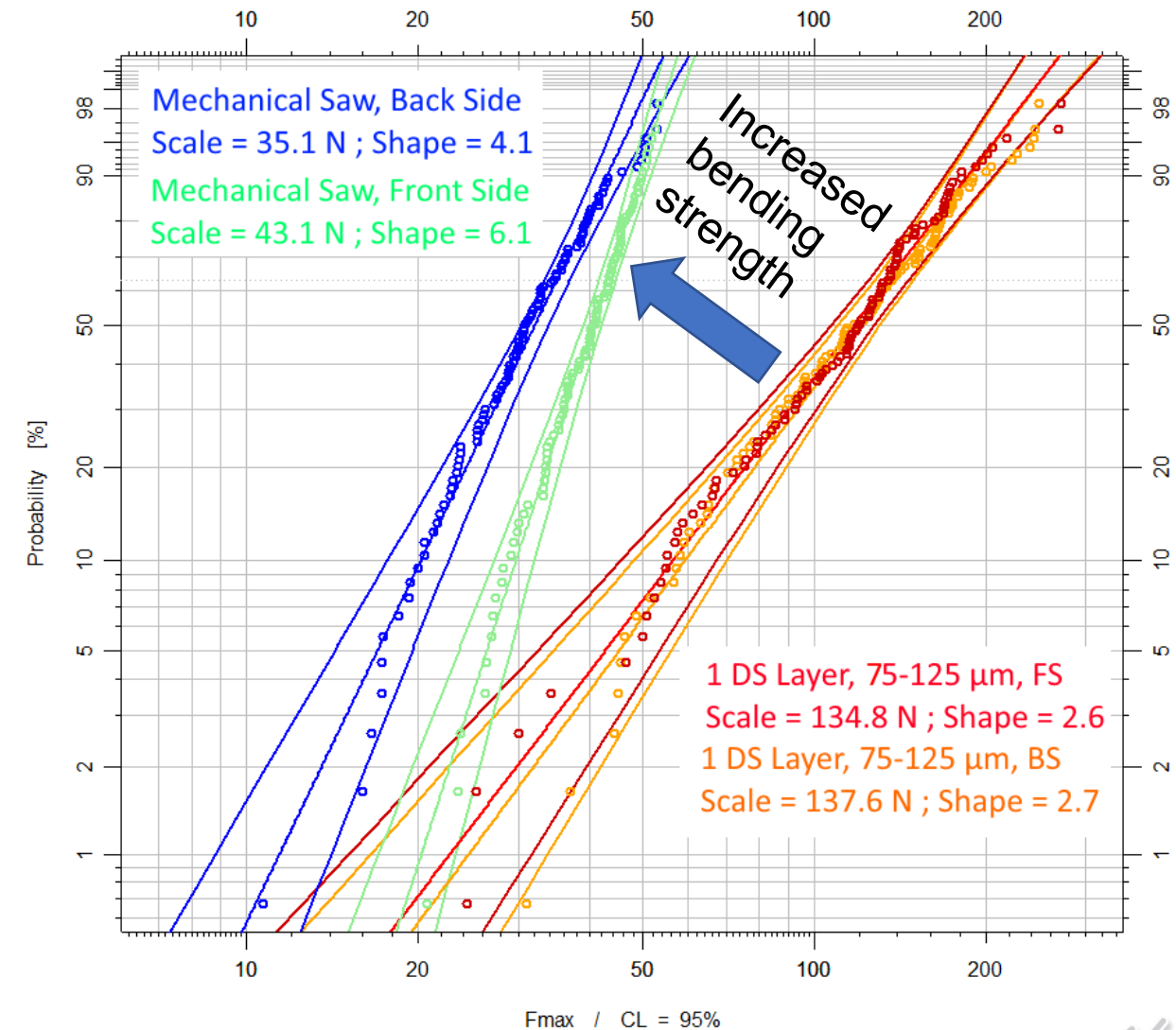


## Mechanical Blade Dicing





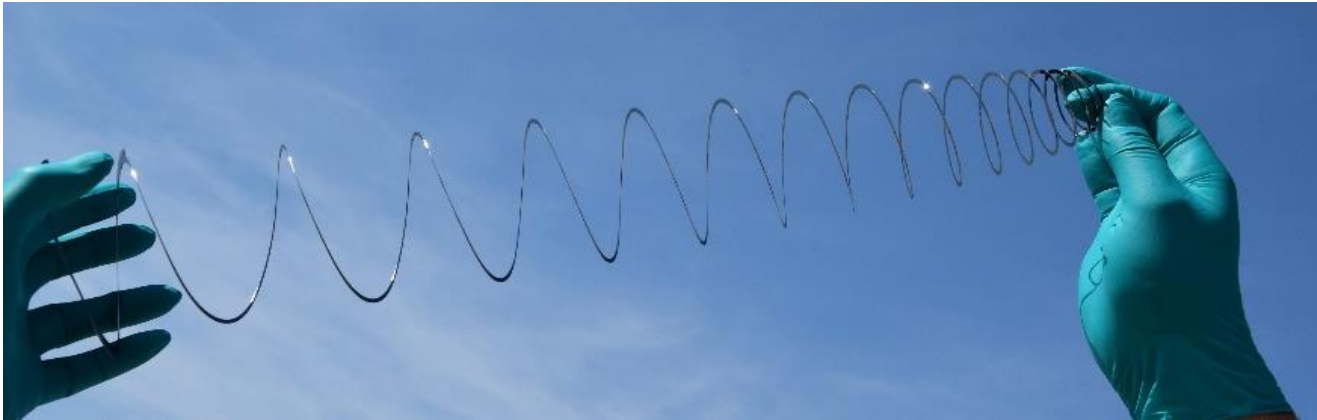
- Shifting to neutral fiber
- Single Layer 75 – 125  $\mu m$ 
  - FS: 134.8 N , BS: 137.6 N
- Mechanical saw
  - FS: 43.1 N , BS: 35.1 N
- Higher bending strength for TLS samples



- Development of a Deep Scribe
- Creation of a FEM simulation
- Deep Scribe supported TLS is able to separate silicon
- Free of particles and reduces crack deviation ( $< \pm 5 \mu m$ )
- Parameter study shows influences and limits
  - Cleaving up to 2 *mm* thick Si by a single Deep Scribe layer
  - Layer stacking is possible
- Optimization of breaking forces by shifting layer
  - >3-times higher stability



## Thank You!



Gefördert durch:



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für Wirtschaft  
und Energie

aufgrund eines Beschlusses  
des Deutschen Bundestages

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in the frame of the  
Important Project of Common European Interest  
(IPCEI).

